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# Design of high efficiency achromatic metalens with large operation bandwidth using bilayer architecture

Yilin Wang<sup>1</sup>, Qingbin Fan<sup>1</sup> and Ting Xu<sup>1,2\*</sup>

Achromatic metalens composed of arrays of subwavelength nanostructures with spatially varying geometries is attractive for a number of optical applications. However, the limited degree of freedom in the single layer achromatic metasurface design makes it difficult to simultaneously guarantee the sufficient phase dispersion and high diffraction efficiency, which restricts the achromatic bandwidth and efficiency of metalens. Here we propose and demonstrate a high efficiency achromatic metalens with diffraction-limited focusing capability at the wavelength ranging from 1000 nm to 1700 nm. The metalens comprises two stacked nanopillar metasurfaces, by which the required focusing phase and dispersion compensation can be controlled independently. As a result, in addition to the large achromatic bandwidth, the averaged focusing efficiency of the bilayer metalens is higher than 64% at the near-infrared region. Our design opens up the possibility to obtain the required phase dispersion and efficiency simultaneously, which is of great significance to design broadband metasurface-based optical devices.

**Keywords:** metalens; metasurface; nanostructure; waveguide

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## Introduction

Dispersion, as one of the most fundamental properties of optical materials, leads to a spatial separation of different wavelengths. As a result, conventional refractive optical components, such as glass lens, always have chromatic aberration. Although such chromatic aberration can be used for spectrometry, it will significantly degrade the image quality in many imaging-related applications. For the correction of chromatic aberration in multi-wavelengths applications, traditional strategy is to integrate different dispersive materials to form an aplanatic or super-achromatic lens system<sup>1</sup>. Nevertheless, this approach inevitably adds weight, complexity and cost to optical devices, which further restricts their applications in some ultracompact systems.

In recent years, metasurface, which is comprised of arrays of subwavelength nanoscatterers with spatially varying geometries, has shown excellent ability to shape the electromagnetic field at will by manipulating its amplitude, phase, and polarization<sup>2-12</sup>. Ultra-compact planar architecture, ease-of-fabrication and high diffraction efficiency make metasurface the excellent candidate for various applications such as holograms<sup>13-19</sup>, metalenses<sup>20-22</sup>, and polarimeters<sup>23,24</sup>. However, metasurface-based functional elements are classified as diffractive devices, which possess severe chromatic aberrations and thus limit their broadband optical operations. In this context, several pioneering researches have been proposed in terms of eliminating the chromatic aberrations of metalens<sup>25-39</sup>. For example, metasurface unit-cells designed for several

<sup>1</sup>National Laboratory of Solid-State Microstructures, Key Laboratory of Intelligent Optical Sensing and Integration and College of Engineering and Applied Sciences, Nanjing University, Nanjing 210093, China; <sup>2</sup>Collaborative Innovation Center of Advanced Microstructures, Nanjing University, Nanjing 210093, China.

\*Correspondence: T Xu, E-mail: [xuting@nju.edu.cn](mailto:xuting@nju.edu.cn)

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discrete operation wavelengths can be multiplexed or stacked to achieve multi-wavelengths, narrow-band achromatic metalenses<sup>25–31</sup>. In addition, based on the integrated-resonant unit elements to compensate the phase dispersion, broadband achromatic metalenses have also been demonstrated<sup>32–40</sup>. Nevertheless, the limited degree of freedom in the single layer achromatic metasurface design makes it difficult to simultaneously guarantee the sufficient phase dispersion and diffraction efficiency. As a result, the operation bandwidth and averaged efficiency of the single layer achromatic metalens are typically smaller than 40% relative to central wavelength and lower than 50%, respectively.

In this work, we propose a new approach to design high efficiency achromatic metalens with large operation bandwidth based on a stacked bilayer architecture. In contrast to the conventional single layer metasurface, two layers of nanostructures in the bilayer configuration are designed to manipulate phase profile and phase dispersion respectively, which would significantly improve the operation bandwidth and efficiency while giving more options for the design. As a proof-of-concept demonstration, we design a Si bilayer metalens working at the near-infrared region, achieving a large continuous achromatic wavelength from 1000 nm to 1700 nm, about 52% operation bandwidth relative to the central wavelength. In addition, the bilayer Si metalens has an averaged diffraction efficiency about 80% at the near-infrared region, and the focusing efficiency at the central wavelength of 1350 nm reaches up to 75%. Our design opens up the possibility to overcome the challenge of improving phase dispersion and efficiency at the same time, which is of great significance to the broadband applications of meta-devices.

## Design of the bilayer achromatic metalens

To realize a high-efficiency achromatic metalens, we use a tightly spaced bilayer metasurfaces architecture, as shown in Fig. 1. For the design of the top layer, the geometric phase is employed to impose a phase profile  $\varphi_{\text{top}}(\lambda_{\text{max}}, x, y)$  on transmitted waves. The generated phase profile only depends on the orientation of a wave-plate-like birefringent rectangular nanopillar, which is insensitive to the wavelength. The bottom layer of the device, composed of cylindrical nanopillars with different diameters, imposes the propagation phase on incident light. The propagation phase modulation is a function of operating wavelength and can provide the appro-

prate phase dispersion  $\Delta\varphi(\lambda, x, y)$  to compensate phase difference between various working wavelengths. It should note that the propagation phase modulation also introduces an additional phase profile  $\varphi_{\text{add}}(\lambda, x, y)$  that would affect the convergence of the incident light. Therefore, the required focusing phase profile  $\varphi_f(\lambda, x, y)$  consists of the geometric phase modulation of the top layer and the propagation phase modulation of the bottom layer. For the case of operating wavelength  $\{\lambda_{\text{min}}, \lambda_{\text{max}}\}$ , the phase profile  $\varphi_{\text{am}}(\lambda, x, y)$  of the whole achromatic metalens can be expressed as:

$$\varphi_{\text{am}}(\lambda, x, y) = \varphi_f(\lambda, x, y) + \Delta\varphi(\lambda, x, y), \quad (1)$$

with

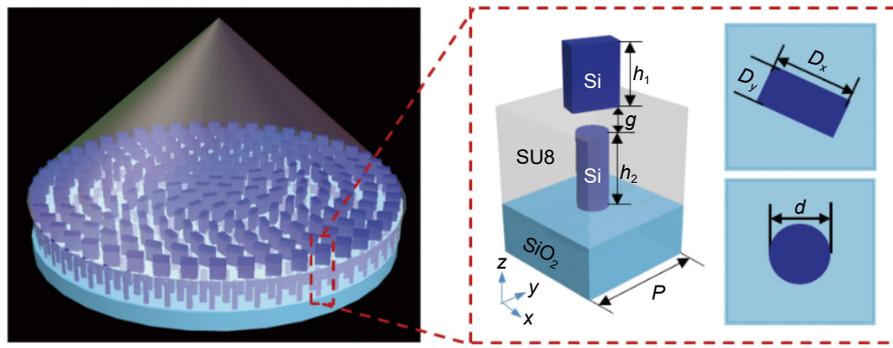
$$\varphi_f(\lambda, x, y) = \varphi_{\text{top}}(\lambda_{\text{max}}, x, y) + \varphi_{\text{add}}(\lambda, x, y), \quad (2)$$

and

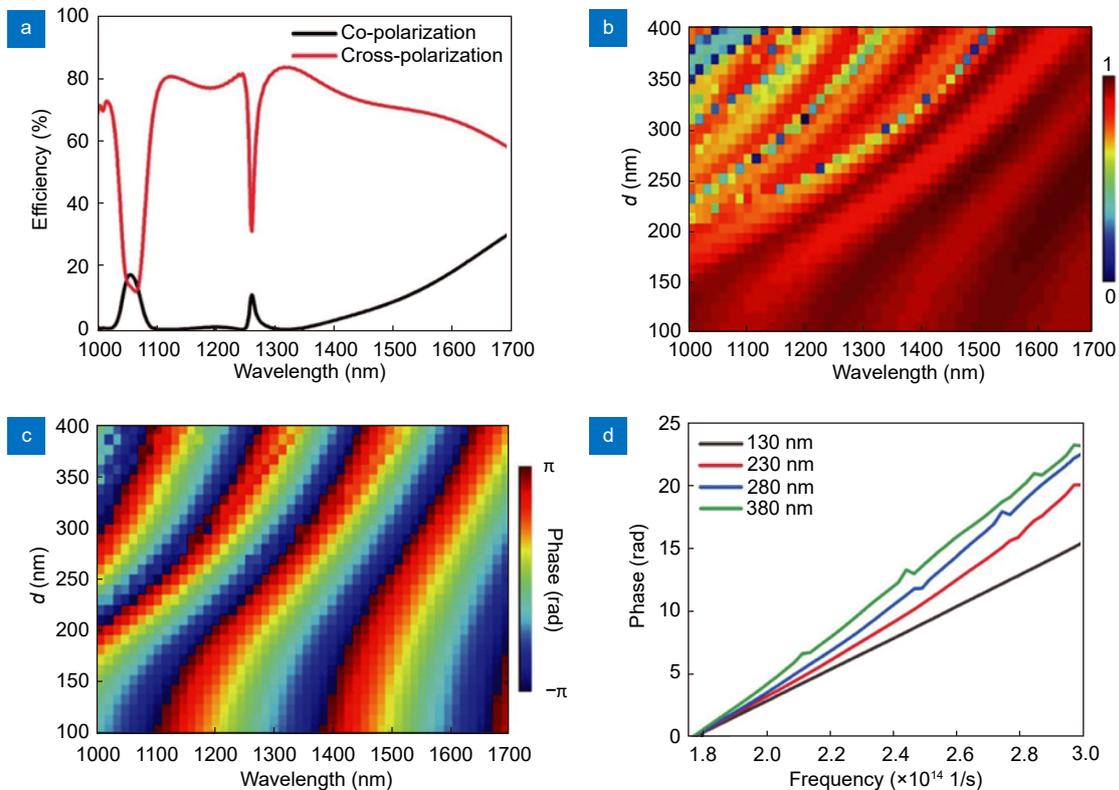
$$\Delta\varphi(\lambda, x, y) = -2\pi \left( \sqrt{x^2 + y^2 + f^2} - f \right) \left( \frac{1}{\lambda} - \frac{1}{\lambda_{\text{max}}} \right). \quad (3)$$

The phase dispersion is only determined by the propagation phase modulation of the bottom layer. The phase profile  $\varphi_{\text{add}}(\lambda, x, y)$  should keep at a relatively low value by optimizing the structure parameters so that the phase profile  $\varphi_f(\lambda, x, y)$  is mainly determined by the geometry phase modulation of the top layer. As a result, in contrast to the single layer achromatic metalens, the proposed bilayer metasurface architecture allows simultaneous realization of broadband response with a large bandwidth and an improved efficiency due to its capability of providing the phase profile and phase dispersion independently.

As a proof-of-concept demonstration, here we use Si nanopillar arrays to design an achromatic bilayer metalens working at near-infrared region. As shown in Fig. 1, each unit cell of the bilayer metalens contains two Si nanopillars. As mentioned before, the top rectangular nanopillar is design to provide basic phase by tailoring the orientations of structure and the bottom cylindrical nanopillar is design to provide phase dispersion by tailoring the diameters of structure, which can ensure large phase dispersion compensation and high efficiency. Considering the feasibility of nanofabrication, the bottom nanopillar is immersed in a polymer photoresist SU8 while the top one is exposed to the air with the gap between them  $g = 400$  nm. The heights for top and bottom nanopillars are  $h_1 = 850$  nm and  $h_2 = 1500$  nm, respectively, with a same square lattice constant  $P = 500$  nm. For incident circularly polarized light, as high



**Fig. 1 | Schematic for bilayer broadband achromatic metalens.** It has the same focal plane over a large continuous wavelength region. Inset: Oblique view of a unit cell of a bilayer Si nanopillars with different heights  $h_1 = 850$  nm,  $h_2 = 1500$  nm, in-plane cross-sectional dimensions  $D_x = 420$  nm,  $D_y = 190$  nm and lattice constant  $P = 500$  nm, on a  $\text{SiO}_2$  substrate. Right: The top view of each layer.



**Fig. 2 | (a)** Simulated polarization conversion efficiency of the top rectangular nanopillar as a function of wavelengths from 1000 nm to 1700 nm. Each nanopillar with 500 nm periods, in-plane cross-sectional dimensions  $D_x = 420$  nm,  $D_y = 190$  nm. **(b, c)** Transmission coefficient and phase map of the bottom cylindrical nanopillar with different diameters  $d$  as a function of wavelength from 1000 nm to 1700 nm. **(d)** Phase spectra for cylindrical nanopillar with four different diameters as a function of frequency.

cross-polarization conversion efficiency is essential for the realization of efficient geometry phase modulation, here we pick up the optimized structural parameters for long and short axis lengths  $D_x = 420$  nm and  $D_y = 190$  nm for the top rectangular nanopillar. As shown in Fig. 2(a), the calculated cross-polarization conversion efficiency of the rectangular nanopillar is relatively high across the near-infrared wavelength range from 1000 nm to 1700 nm expect for two resonant positions. As a res-

ult, by changing the orientation angle of rectangular nanopillar, it can readily provide  $0-2\pi$  geometry phase modulation.

On the other side, for the bottom cylindrical nanopillar, Figs. 2(b) and 2(c) respectively illustrate the calculated transmission coefficient and propagation phase as a function of its diameter  $d$  at near-infrared wavelength region. From Fig. 2(b), it can be clearly seen that the cylindrical nanopillars with different diameters always keep

a high transmission coefficient in the broad spectral range, which is a prerequisite for achieving high efficiency lens. Besides the high transmission coefficient, the Si cylindrical nanopillar with different diameters also exhibits smooth and large phase modulation coverage at the wavelength ranging from 1000 nm to 1700 nm (Fig. 2(c)). From these results, eleven Si cylindrical nanopillars with different diameters are selected to constitute the metasurface. The phase spectra of the four structures are shown in Fig. 2(d). We need to choose smooth and linear structure of the phase spectra to achieve the function of achromatic aberration. The slope in phase spectra also can intuitively reflect the magnitude of phase dispersion. The above method is able to provide sufficient phase dispersion compensation for the design of broadband achromatic metalens. In addition, due to the employment of Si with high refractive index, the coupling effect between neighboring nanopillars is very weak, and thus each nanopillar can be regarded as an isolated waveguide. This makes the phase design for each nanopillar element stay accurate even when they are arranged in a square lattice to form the metalens.

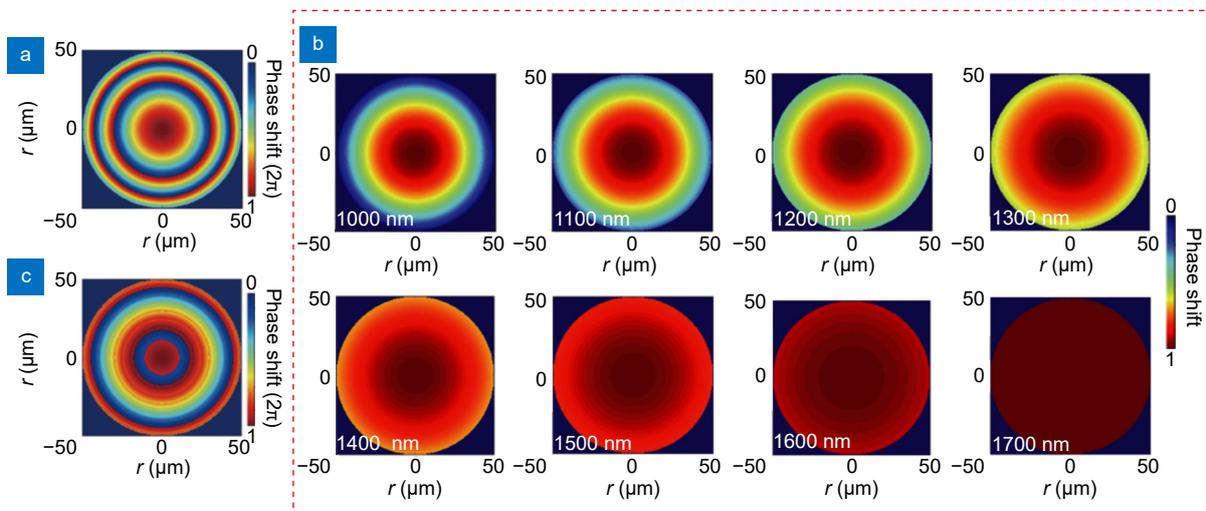
Based on the above approach, we design and demonstrate a bilayer broadband achromatic metalens with  $D = 100 \mu\text{m}$  and  $f = 340 \mu\text{m}$  working at near-infrared wavelength region. The top Si rectangular nanopillars have the same lengths of long and short sides of  $D_x = 420 \text{ nm}$  and  $D_y = 190 \text{ nm}$  but with different orientation angle  $\theta$ . The bottom Si cylindrical nanopillars are designed with the diameter ranging from 130 nm to 380 nm. The ideal phase profile is given in Fig. 3(a), which can theoretically achieve a perfect focusing and is mainly provided by the top layer. As expected, different phase

dispersion compensation can be obtained at the different wavelengths. Fig. 3(b) reveals the bottom layer normalized phase compensation profile at the different wavelengths while it introduces an additional focusing phase. To mitigate the effect of propagation phase on convergence, we expect the  $\varphi_{\text{add}}(\lambda, x, y)$  to be as small as possible under the condition of satisfying the phase dispersion, and thus the optimized phase profile of top layer becomes as shown in Fig. 3(c).

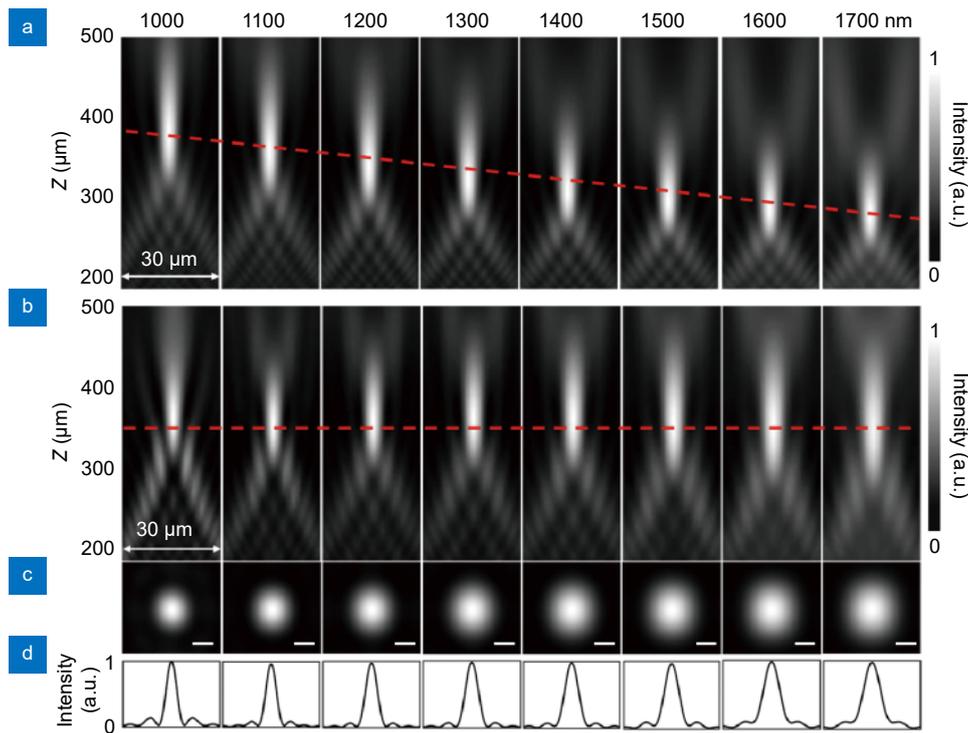
### Characterization of bilayer achromatic metalens

For intuitively exhibiting the achromatic characteristics, bilayer achromatic metalens and single layer chromatic metalens with same diameter and focal length are simultaneously numerically investigated with a right-handed circularly polarized light. Figs. 4(a) and 4(b) denote their intensity profiles simulated along  $x$ - $z$  plane over a wavelength region from 1000 nm to 1700 nm, at a step of 100 nm. In contrast to the chromatic metalens exhibiting a large focal length shift similar to a Fresnel lens with increased incident wavelength (Fig. 4(a)), the bilayer chromatic metalens can converge the incident light with similar focal length at these wavelengths (Fig. 4(b)). Figs. 4(c) and 4(d) shows the simulated focal spot and corresponding cross-section of the intensity profiles at the focal plane, respectively. It can be clearly seen that the focal spot has a circularly symmetric shape and the cross-section exhibits an Airy disk distribution with low side lobes, which demonstrate the good lensing quality of the designed bilayer achromatic metalens.

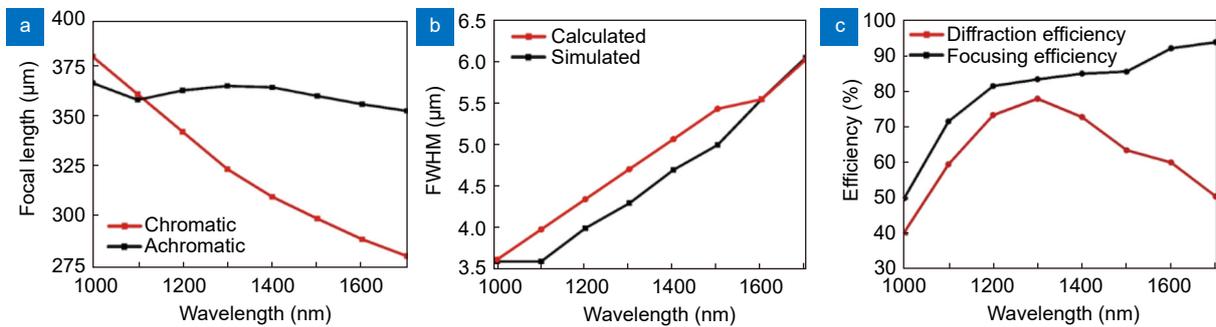
In order to quantitatively reveal the performance of



**Fig. 3 | The phase profile of bilayer achromatic metalens. (a)** The ideal phase profile at the  $\lambda_{\text{max}}$ . **(b)** The bottom layer normalized phase compensation profile over a wavelength region from 1000 nm to 1700 nm, at a step of 100 nm. **(c)** The required phase profile of top layer.



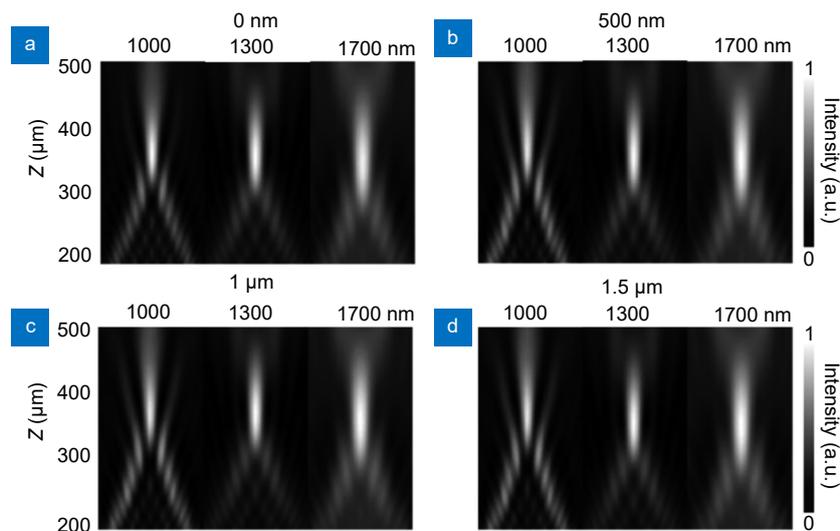
**Fig. 4 | Simulated verification of chromatic and achromatic metalens.** (a, b) Numerical intensity profiles of broadband chromatic (a) and achromatic (b) metalens with NA = 0.15 at various incident wavelengths. The red dashed line indicates the position of the focal plane. (c, d) Normalized intensity profiles along the red dashed lines of (b). Scale bar: 6 μm.



**Fig. 5 | Performance of broadband achromatic metalens.** (a) The focal length shift values of both chromatic and achromatic metalenses as a function of incident wavelength. (b) The FWHM of the focal spots as a function of incident wavelength. (c) The efficiency of achromatic metalens as a function of incident wavelength.

achromatic metalens, Fig. 5(a) shows the focal length shift values of both chromatic and achromatic metalenses as a function of incident wavelength. For the wavelength ranging from 1000 nm to 1700 nm, the focal length shifts more than 100 μm for the chromatic metalens while keeps almost invariable for the bilayer achromatic metalens. As a result, the bilayer metalens achieves the achromatic bandwidth of 700 nm, which is about 52% relative to the central wavelength and larger than that of the single layer one. Fig. 5(b) shows the full-width half-maximum (FWHM) of the focal spots of the bilayer metalens. It can be seen that the simulated

FWHM values are close to the theoretical diffraction-limited values  $\left(\frac{\lambda}{2NA}\right)$  of the designed metalens with NA= 0.15. In addition to the achromatic bandwidth, the bilayer metalens also has high diffraction and focusing efficiency, as shown in Fig. 5(c). The focusing efficiency is defined as the ratio of light intensity from the focal spot to the light intensity of incident beam. Due to the employment of low loss Si as constituent material and the optimization of the geometry parameters for the nanopillar structures, the bilayer metalens has the averaged diffraction and focusing efficiencies about 81% and 64% for the investigated wavelength range, respectively, and



**Fig. 6 | The influence of structural deviations on the lensing quality.** (a) – (d) The simulated focal intensity profiles of bilayer metalens with perfect alignment (a), misalignment of 500 nm (b), 1  $\mu\text{m}$  (c) and 1.5  $\mu\text{m}$  (d) between two metasurface layers at three different wavelengths.

the focusing efficiency can reach up to 78% around the wavelength of 1300 nm. The focusing efficiency decreases quickly at the wavelength longer than 1400 nm, which is mainly attributed to the lower polarization conversion efficiency of the nanopillar. Moreover, although similar efficiency of achromatic metalens has been reported in previous work<sup>40</sup>, it has much larger diameter while our design is more feasible for practical imaging applications. These results imply that the bilayer achromatic metalens proposed here have good performance of correcting chromatic aberration over a continuous wide range of near-infrared wavelength. Our method can also be used to design the high efficiency achromatic metalens with large diameter or high numerical aperture.

Finally, considering the alignment tolerance between two metasurface layers during the fabrication of bilayer metalens, we further investigate the influence of structural deviations on the lensing quality. Figs. 6(a)–6(d) shows the simulated focal intensity profiles of bilayer metalens with perfect alignment, misalignment of 500 nm (one unit cell), 1  $\mu\text{m}$  (two unit cells) and 1.5  $\mu\text{m}$  (three unit cells) between two metasurface layers at three different wavelengths. It can be clearly seen that in all the cases have similar focal intensity profiles and the focal lengths are almost the same. This originates from the fact that the required focusing phase are from the top metasurface layer while the bottom metasurface layer mainly provides dispersion compensation. Therefore, this proposed bilayer achromatic metalens has a robust tolerance for nanofabrication.

## Conclusion

In summary, we propose a new approach to design high efficiency achromatic metalens with large operation bandwidth by the modulation of dispersion using bilayer architecture. Two stacked metasurface layers are designed to separately provide required focusing phase profile and dispersion compensation. As a proof-of-concept demonstration, by using Si rectangular and cylindrical nanopillar arrays, we design a broadband achromatic metalens with 700 nm operation bandwidth and 64% averaged focusing efficiency working at near-infrared region. Compared with conventional achromatic multilevel diffractive elements<sup>41</sup>, our device provides a general approach for achieving multifunctional high pixel density achromatic optics. This method solves the problem of mutual constraint between required phase dispersion and efficiency in single layer metasurface and opens up the possibility to design multifunctional broadband meta-devices.

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## Competing interests

The authors declare no competing financial interests.